

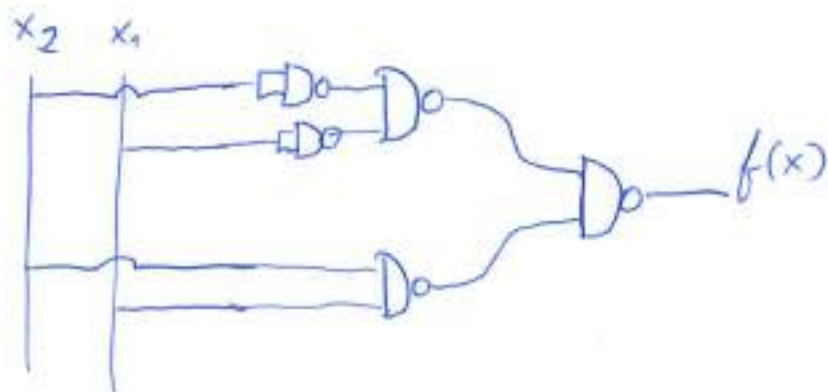
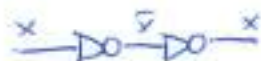
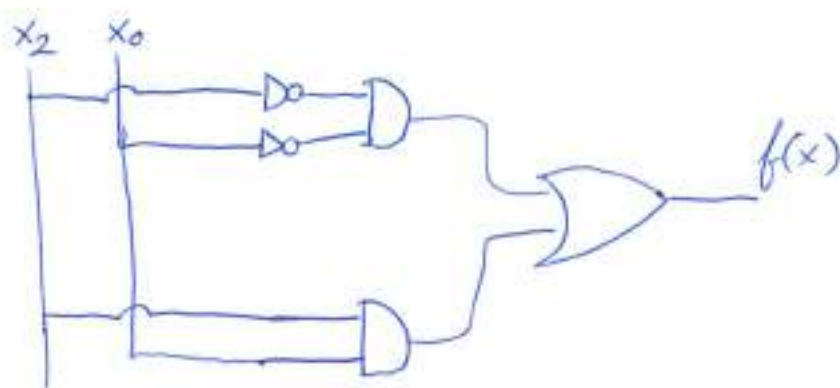
EXAM AUG 20, 2018

A1

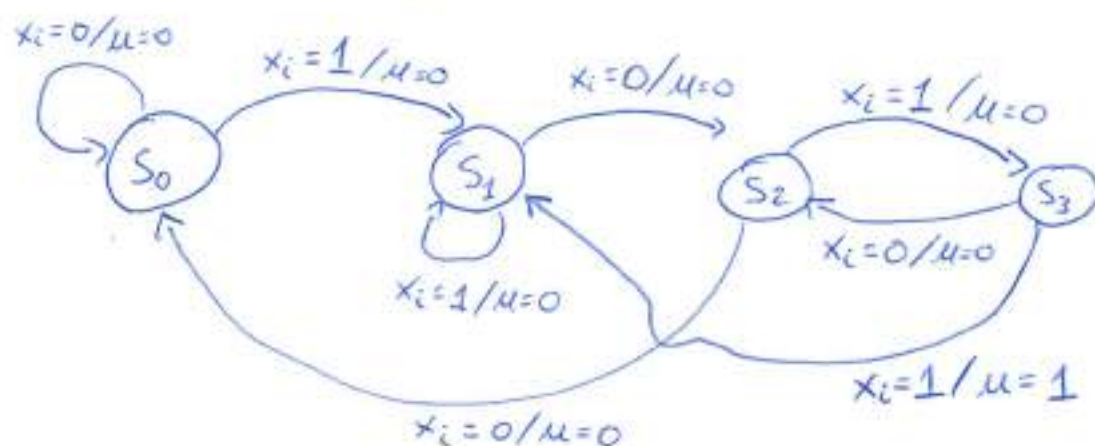
$x_3 \times 2$

		00	01	11	10
$x_1 x_0$	00	1	0	-	1
	01	0	1	1	0
	11	0	1	-	0
	10	1	0	0	-

$$f(x) = \overline{x_0} \cdot \overline{x_2} + x_0 \cdot x_2$$



A2 State diagram



State coding:

	q_1	q_0
S_0	0	0
S_1	0	1
S_2	1	0
S_3	1	1

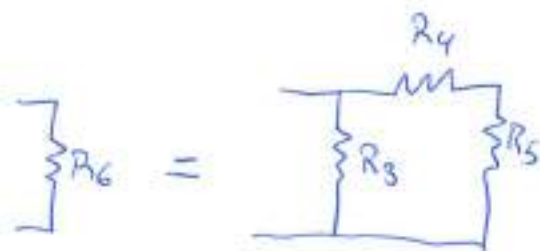
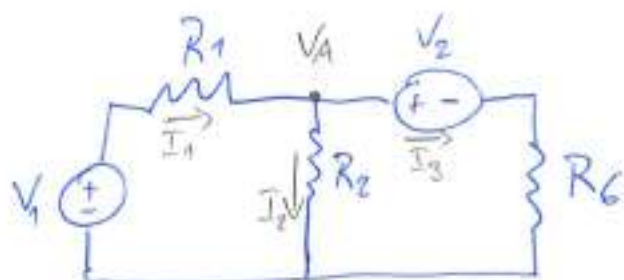
	q_1	q_0	x_i	q_1^+	q_0^+	μ
	0	0	0	0	0	0
	0	0	1	0	1	0
	0	1	0	1	0	0
	0	1	1	0	1	0
	1	0	0	0	0	0
	1	0	1	1	1	0
	1	1	0	1	0	0
	1	1	1	0	1	1

• 2 D flip-flops are used, 1 per

• This is a ~~Mealy~~ Mealy circuit, Since the output μ depends on both the state and the input at each time.

A₃

a)



$$I_1 = I_2 + I_3$$

$$I_1 = \frac{V_1 - V_A}{R_1} ; I_2 = \frac{V_A}{R_2} ; I_3 = \frac{V_A - V_2}{R_6}$$

$$R_6 = R_3 // (R_4 + R_5)$$

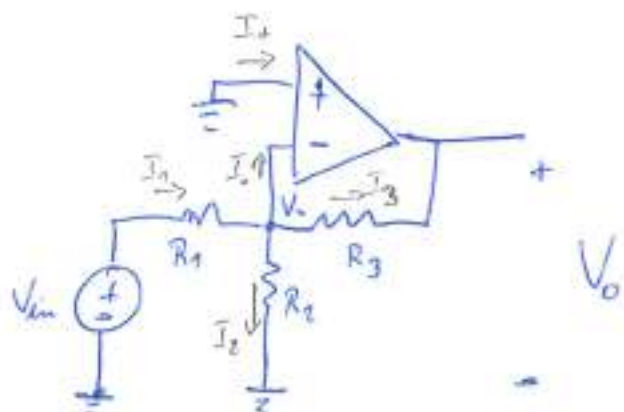
$$= \frac{R_3(R_4 + R_5)}{R_3 + R_4 + R_5} = 10 \Omega$$

$$\Rightarrow \frac{V_1 - V_A}{R_1} = \frac{V_A}{R_2} + \frac{V_A - V_2}{R_6} \quad (\Rightarrow) \quad \left(\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{R_6} \right) V_A = \frac{V_1}{R_1} + \frac{V_2}{R_6}$$

$$\frac{1}{5} V_A = \frac{5}{20} + \frac{2}{10} \quad (\Rightarrow) \quad V_A = \frac{9}{4} \text{ V}$$

$$I_2 = \frac{V_A}{R_2} = \frac{9}{4 \times 20} = \frac{9}{80} \text{ A} = 0.1125 \text{ A}$$

A3.6)



Ideal OPAMP:

- $I_+ = I_- = 0$

- $V_+ = V_-$ (because of negative feedback)

$$V_+ = 0 \Rightarrow V_- = V_+ = 0$$

$$I_1 = \frac{V_{in} - V_-}{R_1} \quad ; \quad I_2 = \frac{V_-}{R_2} \quad ; \quad I_3 = \frac{V_- - V_o}{R_3}$$

$$I_1 = I_2 + I_3 + \cancel{I_-} = I_2 + I_3$$

$$I_2 = \frac{V_-}{R_2} = \frac{0}{R_2} = 0 \Rightarrow I_1 = I_3$$

$$\Rightarrow I_1 = I_3 \quad (=) \quad \frac{V_{in} - \overset{=0}{V_-}}{R_1} = \frac{\overset{=0}{V_-} - V_o}{R_3} \quad (=) \quad V_o = -\frac{R_3}{R_1} V_{in}$$

$$\Rightarrow I_3 = I_1 = \frac{V_{in} - \overset{=0}{V_-}}{R_1} = \frac{3}{100} = 30 \text{ mA}$$

AU

a) $R_B = 10 \text{ k}\Omega$

$R = 200 \Omega$

$V_{CE} = ?$

$V_{in} = 5 \text{ V}$

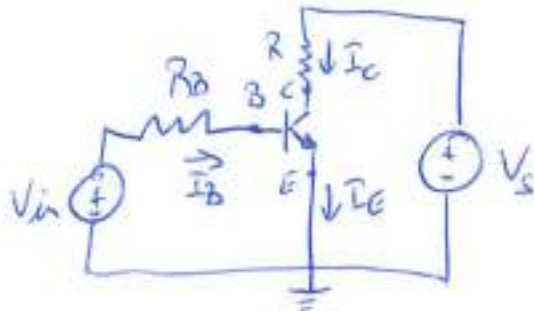
$I_E = ?$

$V_S = 12 \text{ V}$

$I_C = ?$

$V_{BE} = 0.6 \text{ V}$

$\beta = 100$



• $V_{BE} = V_B - \overset{=0}{V_E} = 0.6 \text{ (}\Rightarrow\text{)} V_B = 0.6 \text{ V}$

• $I_B = \frac{V_{in} - V_B}{R_B} = \frac{5 - 0.6}{10 \text{ k}} = \frac{4.4}{10^4} = 0.44 \text{ mA}$

• $I_C = \beta I_B = 44 \text{ mA}$; $V_C = V_S - R I_C = 12 - 8.8 = 3.2 \text{ V}$

$V_{CE} = V_C - \overset{=0}{V_E} = V_C = 3.2 \text{ V}$

• $I_E = I_C + I_B = 44.44 \text{ mA}$

A4. b) Saturation mode ; $V_B > V_E$ and $V_{CE} < V_{CE, \text{sat}}$
 $R_B = ?$

From a): $V_{CE} = V_C - V_E = V_C$; $V_C = V_S - R I_C =$
 $= 12 - 200 I_C$

$$I_C = \beta I_B \Rightarrow V_{CE} = 12 - 200 \beta I_B$$

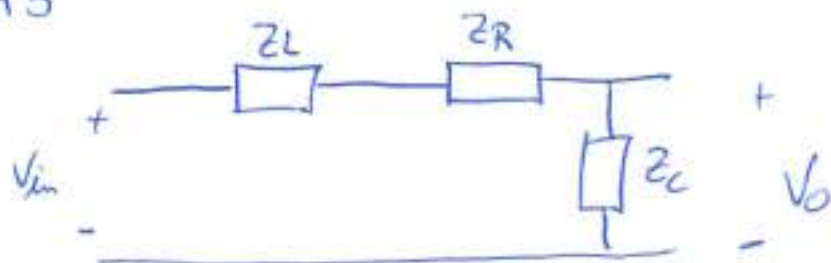
$$I_B = \frac{V_{in} - V_{BE}}{R_B} = \frac{4.4}{R_B}$$

$$\Rightarrow V_{CE} = 12 - 2 \times 10^4 \times \frac{4.4}{R_B}$$

$$V_{CE} < V_{CE, \text{sat}} \Rightarrow V_{CE} < 0.2V \Rightarrow 12 - \frac{8.8 \times 10^4}{R_B} < 0.2 \Rightarrow$$

$$R_B < \frac{8.8 \times 10^4}{12} \Omega$$

A5



V_{in} and V_o
are phasors, where
 $V_{in}(t) = \text{Im}(V_{in} e^{j\omega t})$

$$V_{in} = 2 e^{j\frac{\pi}{3}} ; \omega = 2\pi f = 8000\pi \text{ rad/s}$$

$$V_o = H(j\omega) V_{in} ; H(j\omega) = ? \Rightarrow H(j\omega) = \frac{Z_C}{Z_L + Z_R + Z_C}$$

$$Z_R = R = 50 \Omega ; Z_L = j\omega L = j\omega \text{ m}\Omega$$

$$Z_C = \frac{1}{j\omega C} = \frac{1}{j\omega \times 1.6 \times 10^6} \Omega$$

$$H(j\omega) = \frac{\frac{1}{j\omega C}}{j\omega L + R + \frac{1}{j\omega C}} = \frac{1}{(j\omega)^2 LC + j\omega RC + 1} =$$

$$= \frac{1}{1 - \omega^2 LC + j\omega RC} = \frac{1}{1 - 64\pi^2 \times 10^6 \times 1.6 \times 10^{-9} + j 8\pi \times 5 \times 10^{-2}}$$

$$H(j\omega) = \frac{1}{1 - 64\pi^2 \times 1.6 \times 10^{-3} + j 4\pi \times 1.6 \times 10^{-1}} = -0.0026 - j0.4973$$

($\omega = 8000\pi$)

$$V_o = H(j\omega) V_{in} = |H(j\omega)| |V_{in}| e^{j(\arg(H(j\omega)) + \arg(V_{in}))}$$

$$= 0.4974 \times 2 e^{j(-1.58 + \frac{\pi}{3})}$$

$$V_o(t) = 0.995 \times \sin(8000\pi t + \frac{\pi}{3} - 1.58)$$

